

Seminário de Encerramento do Projeto

SeismicPRECAST - "Seismic performance Assessment of existing Precast Industrial buildings and development of Innovative Retrofitting sustainable solutions"

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SeismicPRECAST - "Seismic performance ASSessment of existing Precast Industrial buildings and development of Innovative Retrofitting sustainable solutions"



Seismic Performance Assessment of Existing Precast Industrial Buildings and Development of Innovative Retrofitting Sustainable Solutions POCI-01-0145-FEDER-028439

Avaliação sísmica de estruturas existentes pré-fabricadas de betão armado

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SeismicPRECAST - "Seismic performance Assessment of existing Precast Industrial buildings and development of Innovative Retrofitting sustainable solutions"

- Task 1 | State-of-art review and initial studies
- Task 2 | Typical properties of the Portuguese precast industrial buildings
- Task 3 | Development of a Vulnerability Model
- Task 4 | Development and validation of retrofitting solutions
- Task 5 | Life-Cycle assessment of seismic retrofit strategies applied to existing precast RC Structures
- Task 6 | Integration of the data, development of guidelines and application to real case studies
- Task 7 | Project management and organization of scientific and technical meetings



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Characterization of the Portuguese Industrial Building Park Geographical distribution

- Comparison between the location of the collected projects and the actual manufacturing industry according with the data available in Pordata
- The buildings tend to be concentrated at the <u>center and</u> <u>northern regions of the Portuguese coast side</u>







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Characterization of the Portuguese Industrial Building Park



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Characterization of the Portuguese Industrial Building Park

Beam-to-column connection

- In 60 % of the cases it was possible to access the details about the dowel connection
- Variability in terms of the number and diameter of the dowels
- The area of the dowels appears to be correlated with the beam span
- Regarding the corbel properties the results obtained from the data collected reveal values that vary between 10 and 50 cm
- The corbel span seems to be independent of the longitudinal beam span





Columns reinforcement ratio

n [m]

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20 30 4 Corbel span [cm]



Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level

- Existing Precast Industrial framed structure (180 ×175 m²)
- · Height: 12 m
- 5 Spans in the X direction with 35 m of length
- 15 Spans in the Y direction with 12 m of length
- Concrete C40/50
- Steel S500 NR-SD



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Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level



Seismic Assessment of Precast Buildings

Beam-to-column connection

• To access the accuracy of the numerical model, each experimental test was simulated considering the set of parameters previously defined



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Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level

Parametric Study

- Several cases were considered in a 3D model to better understand the impact that certain parameters have on the response of the building
- The parameters considered are focused on the response of the beam-to-column connections, namely regarding the relative importance of the <u>contribution of the dowels</u>, <u>neoprene and friction</u>

	Number/Diamete		Neoprene Pad [mm]			
Model	X Direction Y Direction				Friction	
PC		Pinned Connection				
DFNC	<mark>2 Ø24</mark>	<mark>2 Ø20</mark>	<mark>Yes</mark>	<mark>20</mark>		
DC	2 Ø24	2 Ø20	NC NC	NC NC		
FNC	NC	NC	Yes	20		
NC- not considered in the model						



Neoprene

Pad [mm]

Friction

Yes

NC

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Seismic Assessment of Precast Buildings Beam-to-column connection – Influence at the buildings level

DFNC And Pinned connection

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- Comparing the model with a connection with dowel, friction and neoprene and a model with pinned connections (usually considered in the common design stage)
 - · The difference is very low, which shows that developing a detailed connection model might not be necessary to study the drifts and seismic coefficients of the structure
 - · Most of the time, the DFNC model leads to slightly higher results when compared with the PC model

Model

PC

DFNC

2 Ø24

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Model

DFNC

DC

Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level

Effect of the neoprene and friction

- · Evaluate the effect of the connection only with the dowel (DC) and the connection considering the dowel, friction and neoprene (DFNC)
 - Difference between these model connections is inexistent | Low influence of the friction and neoprene in the drift and seismic coefficient of the structure
 - · For buildings with higher demands at the connection level, the contribution of the friction and neoprene pad may not be so

X Direction

2 Ø24

2 Ø24

Number/Diameter of Dowels [mm]

Y Direction

2 Ø20

2 Ø20

insignificant

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Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level

Effect of the dowels

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- Significant difference between considering FNC and DFNC connections
 - The dowel is a connection parameter with influence in the drift and seismic coefficient of the structure
 - For the same PGA, the model without dowel presents a lower drift demand in the columns when compared with the model with dowels

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	Number/Diameter of Dowels [mm]		Neoprene			0.02		101100-000	-			-
Model	X Direction	Y Direction	Friction	Pad [mm]		0.00	1 02	0.3	0.4	0.5	0.6	
DFNC	<mark>2 Ø24</mark>	<mark>2 Ø20</mark>	Yes	20		0.0		010		0.0	0.0	
FNC	NC	NC	Yes	20		-61	-	Datu				
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								PG	0CI-0	1-01	45-F	46

MAX DPNC H MAX DPNC C MAX PNC C D PN



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Seismic Assessment of Precast Buildings

Beam-to-column connection – Influence at the buildings level

- The results showed the <u>importance of the beam-to-column connections</u> to the seismic behaviour of the entire structure
- If the dowels are well designed, <u>small deformations are expected at the connections level</u> and, therefore, the response of the structures is controlled by the properties of the vertical elements
- For these cases, the consideration of <u>simple pinned connection appears as an efficient and accurate</u> <u>numerical approach</u>
- On the other hand, in the <u>absence of dowels</u>, or in cases where these are not properly designed, a <u>concentration of damage is expected to occur at the connection level</u>, while the columns remains essentially undeformed
- Hence, whenever the relative horizontal strength between the columns and the adjacent connections is unknown, the consideration of the different connection mechanisms is recommended in order to obtain a reliable estimation of the seismic behavior of the building

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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3

Objectives:

Seismic assessment using nonlinear static (pushover) and dynamic analyses, following the recommendations presented on Eurocode 8 – Part 3.

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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3

Structures information							
	Structure ID	Year	Seismic Zone				
Mid code	B3_ModC	1997	1.2				
Pre code	B5_PreC	1979	1.5				

- The existing PRC **buildings** considered to perform the **seismic assessment**, following the prescriptions of the **Eurocode 8 Part 3** were **collected from the database**
- The buildings were chosen with the objective of reflecting the typical properties on each period
- It was decided to define three sub-classes based on the year of construction, as an important fraction of the mechanical and geometric properties depend on the year of construction
- The sub-classes were defined as:
 - 'Pre code': 1960 to 1980
 - '*Moderate code*': 1980 to 2000
 - 'Post code': 2000 to 2020

Buildings distribution vs Type 1 seismic zonation



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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3





Columns

Geometric characteristics of the buildings in studying

Structure	Number of spans		Span length		Height	Slenderness			
ID	x	у	x [m]	y [m]	[III]	x	у]	
B3_ModC	8	8	17.0	6.0	9.0	69	89		
B5_PreC	2	10	15.0	4.2	7.5	65	65	1	

Material and reinforcement detailing

D 111 ID	Concrete	Steel f _{vm}	characterization Column	%	Dowel	
Building ID	f _{cm} [MPa]	[MPa]	bxh [m]	Longitudinal	Transversal	Ø [mm]
B3_ModC	33	440	0.45x0.35	1.60	0.17	2Ø16
B5_PreC	24	440	0.40x0.40	0.79	0.16	-

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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3

Nonlinear static analysis

- The assessment of the buildings was firstly carried out through nonlinear static (pushover) analyses
- These analyses were carried out along the two main directions of the buildings adopting a distribution of incremental horizontal forces proportional to the shape of the fundamental modes and a uniform distribution proportional to the mass, according with the Eurocode 8 recommendations
- The effects of the accidental eccentricity was also considered in order to account for possible variations in the distribution of masses in the structures
- The **normative resistance** for the **flexural** and **shear mechanisms** was calculated, along with the appliance of the N2 method, as defined in the Eurocode 8
- The determination of the target displacement associated with the seismic hazard at the building location was based on the procedure presented on the Annex B of Eurocode 8 – Part 1

Pushover curves for B5 PreC

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Assessment of existing RC precast industrial buildings according with Eu

Building assessment - Static analysis

- Almost perfect overlapping of the pushover curves associated with the uniform and modal distributions \rightarrow single-story buildings and regular in plan
- Both building appear to fulfil the code requirements given that the target displacement associated with the seismic zone 1.3 is lower than the displacement associated with the exceedance of the elements chord rotation and shear capacity
- The latter mechanism (ultimate chord) is very unlikely to occur given the large slenderness of the columns
- Building could be classified as seismically safe



- Expressions applied only in the column (beams should remain essentially undamaged)
- Beam-to-column connection: limit of 6 cm of relative displacement (Cornali et al.)

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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3

Building assessment – Structural capacity

- Capacity of the buildings → Eurocode 8 Part 3
- Significant damage (SD) limit state
- $\theta_{um} = \frac{3}{4} \frac{1}{\gamma_{-1}} 0,016 \cdot (0,3^{\nu}) \left[\frac{\max(0,01;\omega')}{\max(0,01;\omega)} f_c \right]^{0.225} \left(\min\left(9; \frac{L_{\nu}}{h}\right) \right)^{0.35} 25^{\left(\alpha \rho_{SX} \frac{f_{yw}}{f_c}\right)} (1,25^{100\rho d})$ • Chord rotation (deformation)
- $V_{R} = \frac{1}{2L} \left[\frac{h-x}{2L} \min(N; 0.55A_{c}f_{c}) + (1-0.05\min(5; \mu_{\Delta}^{pl})) \cdot \left[0.16\max(0.5; 100\rho_{tot}) \left(1-0.16\min(5; \frac{L_{v}}{h}) \right) \sqrt{f_{c}}A_{c} + V_{w} \right] \right]$ Shear strength

 $\gamma_{el} \lfloor 2L_{v} \rfloor$		









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Assessment of existing RC precast industrial buildings according with Eurocode 8 - Part 3

Building assessment – Static analysis

- Similar results were attained considering the behaviour at the beam-to-column connection → presence of steel dowels that prevent the connection to fail under seismic loads
- Connection ensured by friction → potential failures under moderate to high seismic loads
- Based on a limit differential displacement at the beam-to-column connections of 6 cm for severely damaged connections, it was possible to verify that for the model B5_PreC (pre code design) the connection fail for a global displacement lower than the one associated with the ultimate chord rotation
- Although the connection limit state occurs for a global displacement larger than the target displacement the results points for a potentially vulnerable seismic behaviour









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Influence of cladding panels in the seismic behaviour of a PRC Industrial Building

- <u>Critical problems</u> in the connections of <u>cladding panels on industrial PRC</u> structures in Italy and Turkey <u>during recent earthquakes</u>;
- Non-structural damages and collapse related with high economic losses;
- Making use of a simplified macro element;

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- Assesses the seismic <u>capacity of common claddings-to-structure connections</u> and interaction with main structure;
- Study of a <u>representative building</u> of the Portuguese industrial park.

Influence of cladding panels in the seismic behaviour of a PRC Industrial Building

Precast buildings in Portugal

- <u>Horizontal</u> cladding panels are the most current layout.
- Typical commercial connections in use in Portugal;
- Isostatic Sliding-Frame system for horizontal panels.



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Influence of cladding panels in the seismic behaviour of a PRC Industrial Building

Cladding panels Modelling

 A macro element proposed to simulated <u>the global behaviour at the centre of the</u> <u>frame</u> and connected to the column edges through four diagonal truss elements, with rigid behaviour.





Seismic Assessment of Precast Buildings

Cladding-to-column connection

> The planning of the experimental campaign focuses on claddingstructure connection of horizontal panels.

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- > A better understanding on the behavior of the connection between precast cladding panels and the main structure used in Portugal.
- The results more reliable to calibrate the numerical models.
- Explore the solutions for connections retrofitting.



Instrumentation Setup



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Influence of cladding panels in the seismic behaviour of a PRC Industrial Building

Cladding panels Modelling - Non-linear static analysis

- Different load distributions were applied in the • pushover analysis, a uniform and modal distribution;
- In X direction it is apparent that the presence of the cladding panels has a minor contribution;
- In Y direction the strength and stiffness increases significantly - only one of the three frames does not include the panels.

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